CEV426 Environmental Remediation Spring 2016 FINAL EXAM 30.05.2015 (75 minutes)

Student ID# : Name :

Please read and sign the below statement:

I have read and understood the exam conduct rules of the School of Engineering before starting my exam.

Signature:

Question 1 (12%)

Fill in the blanks. Use one of the candidate terms given below for each blank.

retardation adsorption dissolution volatilization advection dispersion biodegradation vapor pressure solubility octanol-water partition coefficient Henry's law constant

Volatile organic compounds in a vadose zone may be present in four phases:

(1) in the soil moisture due to,

(2) on the soil grain surface due to,

(3) in the pore void due to,

(4) as the free product.

If the free product phase is present, the vapor concentration in the pore void can be estimated from Raoult's law using the compound's and mole fraction.

During the transport of contaminants in an aquifer, delays the advance of the solute front, whereas reduces the peak value.

Question 2 (5%)

Contaminants that have been in the ground for a long period of time are able to diffuse into the less permeable zones of porous media aquifers and into the bedrock matrix of fractured rock aquifers.

Pump-and-treat systems are inefficient in removing these contaminants. Why?

Question 3 (18%)

For an aquifer solid with a bulk density of 2 g/cm³ containing 0.5% organic carbon, estimate the retardation factor for the common polycyclic aromatic hydrocarbon (PAH) naphthalene $(C_{10}H_8)$, used in mothballs.

If the porosity of the aquifer is 0.24, the hydraulic conductivity is 10^{-3} cm/sec, and the hydraulic gradient is 0.001, how fast will a plume of naphthalene travel?

Question 4 (30%)

Groundwater is contaminated with gasoline. The average dissolved gasoline concentration of the groundwater samples is 20 mg/L. In situ bioremediation is being considered for aquifer restoration. The aquifer has the following characteristics:

- Porosity = 0.35
- Organic content = 0.02
- Bulk density of the aquifer materials = 1.6 g/cm^3

Determine:

- a) Contaminant concentration adsorbed to the aquifer solids assuming equilibrium partitioning.
- b) Total contaminant mass in 1 m³ of aquifer.
- c) For 1 m³ of aquifer, the mass of oxygen required to support biodegradation of intruding gasoline.

(Assume 3.08 g of oxygen is required for the complete biodegradation of 1 g of gasoline.) (Data for gasoline is not available. You may use the data of one of the common components in gasoline, such as toluene.)

Question 5 (15%)

A community is installing a new well in a regionally confined aquifer with a transmissivity of $150 \text{ m}^2/\text{day}$ and a storativity of 0.0004. The planned pumping rate is 2000 m³/day. Compute the theoretical drawdown caused by the new well after 30 days of continuous pumping at 1000 m distance.

Question 6 (30%)

A subsurface is contaminated by a spill of 1,1,1-trichloroethane (1,1,1-TCA). The average TCA concentration of the soil samples, taken from the impacted zone is 2000 mg/kg, and no free-product phase is present.

The subsurface has the following characteristics:

- Porosity = 0.4
- Organic content in soil = 0.02
- Degree of water saturation = 30%
- Dry bulk density of soil = 1.6 g/cm^3
- Total bulk density of soil = 1.8 g/cm^3

Soil-vapor extraction is being considered for the remediation of the impacted zone. Estimate the extracted soil-vapor concentration at the start of the remediation project. Report the soil-vapor concentration in units of both **mg/L** and **ppmV**.

Chemical	Molecular Formula	Molecular weight (g/mole)	Henry's law constant (dimensionless)	log K _{ow}	Saturated Vapor Pressure (atm)
Naphthalene	$C_{10}H_8$	128	0.049	3.36	0.0003
Toluene	C_7H_8	92	0.28	2.69	0.037
1,1,1 TCA	$C_2H_3Cl_3$	133	0.77	2.48	0.13
Naphthalene		1,1,1 T CI CI-C-C CI CI	1,1,1 TCA CI H CI-C-C-H CI H		le 1 ₃

CHEMICAL PROPERTIES YOU MAY NEED:

SOME EQUATIONS YOU MAY NEED:

Relationship between Koc and Kow

K = 0.63K	K_{oc} : Organic carbon partition coefficient (L/kg)
$\mathbf{n}_{oc} = 0.05 \mathbf{n}_{ow}$	K_{aw} : Octanol-water partition coefficient (L/kg)

Darcy's Law

<i>dh</i>	Q : volumetric discharge (L ³ /T) K : hydraulic conductivity (L/T)
$Q = -KA\frac{dM}{dl}$	<i>A</i> : cross-sectional area (L^2) <i>dh</i> / <i>dl</i> : gradient of hydraulic head (L/L)

Retardation

	<i>R</i> : Retardation factor $\left[(M/L^3)/(M/L^3) \right]$
$R-1+K$ $\frac{\rho_b}{\rho_b}$	K_d : Distribution coefficient (L ³ /M)
$\mathbf{R} = \mathbf{I} + \mathbf{R}_d$ n	ρ_b : Bulk density (M/L ³)
	n : Porosity (L^3/L^3)

SOME MORE EQUATIONS YOU MAY NEED:

Theis Equation (Nonequilibrium Equation) for Flow in a Completely Confined Aquifer

$h_0 - h = \frac{Q}{4\pi T} \times W(u)$	$egin{array}{c} Q \ h \end{array}$: Constant pumping rate $(L^3 / T; m^3/d)$: Hydraulic head at distance <i>r</i> at time <i>t</i> (L; m)
W(u) : Well function $W(u) = -0.5772 - \ln u + u - \frac{u^2}{2 \cdot 2!} + \frac{u^3}{3 \cdot 3!} - \frac{u^4}{4 \cdot 4!} + \dots$: Initial hydraulic head (L; m)
		: Drawdown (L; m)
22.JJ. + +.	Т	: Aquifer transmissivity (L^2/T ; m^2/d)
$u - \frac{r^2 S}{r^2}$	t	: Time since pumping began (T; d)
$u = \frac{1}{4Tt}$	r	: Radial distance from the pumping well (L; m)
for $u < 0.1$: $W(u) = -0.5772 - \ln u$	S	: Aquifer storativity (-)